

$\text{Al}_{0.8}\text{In}_{0.2}\text{As}_{0.23}\text{Sb}_{0.77}$ Avalanche Photodiodes

Ann-Katheryn Rockwell*, Yuan Yuan*, Andrew H. Jones, Stephen D. March, Seth R. Bank, and Joe C. Campbell

Abstract — We report avalanche photodiodes (APDs) fabricated from the digital alloy $\text{Al}_{0.8}\text{In}_{0.2}\text{As}_{0.23}\text{Sb}_{0.77}$ (lattice-matched to GaSb). The APDs exhibit high avalanche multiplication, and low excess noise.

Index Terms — Avalanche photodiodes, photodetectors, optoelectronic devices

I. INTRODUCTION

Avalanche photodiodes have been widely used in telecommunication, military, and research applications. Relative to p-i-n photodiodes, APDs can provide higher receiver sensitivity owing to their internal gain [1], [2]. However, the gain, which originates from impact ionization, is also the source of noise for which the figure of merit is the excess noise factor $F < M >$. In the local field model [3], the excess noise factor can be expressed as: $F < M > = kM + (1 - k)(2 - 1/M)$, where k is ratio of the hole ionization coefficient, β to the electron ionization coefficient, α , and M is multiplication gain. While the excess noise factor increases with gain, it increases more slowly for low values of k . Thus, k becomes a secondary figure of merit to describe the noise of the APD. Therefore, it is advantageous to utilize materials with low values of k . Another important figure of merit is the gain-bandwidth product. Emmons has shown that smaller k also enables higher gain-bandwidth products [4]. Recently, Shiyu Xie *et al.* have reported that AlGaAsSb APDs, whose k value is ~ 0.1 , exhibit a high gain-bandwidth product of 424 GHz [5], [6].

In this work, we demonstrate an $\text{Al}_{0.8}\text{In}_{0.2}\text{As}_{0.23}\text{Sb}_{0.77}$ p-i-n structure APD that achieves k value < 0.07 , multiplication gain > 480 , and low dark current.

II. DEVICE STRUCTURE AND FABRICATION

Previously, we have demonstrated the high quality growth of $\text{Al}_x\text{In}_{1-x}\text{As}_y\text{Sb}_{1-y}$ digital alloys lattice matched to GaSb for use in staircase, SACM and p-i-n APDs with $x = 0.3-0.7$. In this work, we extend our study of p-i-n APDs to include $x = 0.8$. The $\text{Al}_{0.8}\text{In}_{0.2}\text{As}_{0.23}\text{Sb}_{0.77}$ (written as $\text{Al}_{0.8}\text{InAsSb}$ in the following) epitaxial layers were grown on n-type Te-doped GaSb (001) substrates by solid-source molecular beam epitaxy. The 10 monolayer (ML) or 3.05 nm, period digital alloys were

grown comprising four binary alloys AlSb, AlAs, InSb, and InAs. The resulting shutter sequence was AlSb, AlAs, AlSb, InSb, InAs, Sb [7], [8], [9].

A cross-sectional schematic of the $\text{Al}_{0.8}\text{InAsSb}$ p-i-n structure APD is shown in Fig. 1. From the top to bottom, the structure consists a 100 nm GaSb p-type top contact layer, a 100 nm $\text{Al}_{0.8}\text{InAsSb}$ p-type layer, a 1000 nm $\text{Al}_{0.8}\text{InAsSb}$ unintentionally-doped multiplication layer, a 100 nm $\text{Al}_{0.8}\text{InAsSb}$ n-type layer, a 100 nm GaSb n-type bottom contact layer, and an n-type GaSb substrate. The top three layers are p-type doped using Be, and the other layers are n-type doped with Te.

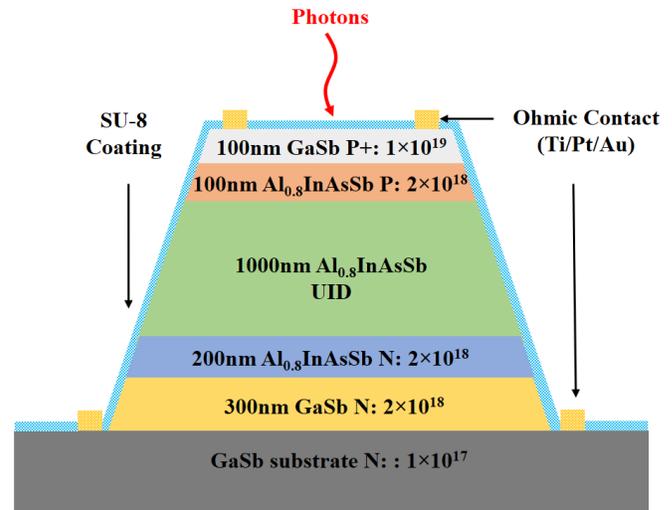


Figure 1. Schematic cross section of $\text{Al}_{0.8}\text{InAsSb}$ p-i-n APD.

The mesas were defined by standard photolithography and formed by wet etching in a 5:1:5 solution of HCl:H₂O₂:H₂O. Ti/Pt/Au was deposited as the top and bottom contacts by electron-beam evaporation [10], [11]. After lift-off of the metals, SU-8 was spun on the sidewall as a surface passivation.

III. RESULTS AND DISCUSSION

In this paper, all measurements were carried out at room temperature. Figure 2 shows the photocurrent, dark current, and gain versus bias voltage of a 100 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ p-i-

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n APD. The APD was illuminated with 10 μW 850 nm laser, and the gain curve is plotted by choosing the unity gain point at -24.5 V. High gain of 489 was achieved at -32.5 V bias. There are three slopes in the photocurrent: the first gradual slope (from 0 to 11 V) might be caused by the heterojunction barrier [12], the second slope (from 11 to 24.5 V) is because of changes in carrier collection efficiency, and after 24.5 V the multiplication gain makes the third slope of the photocurrent steeper.

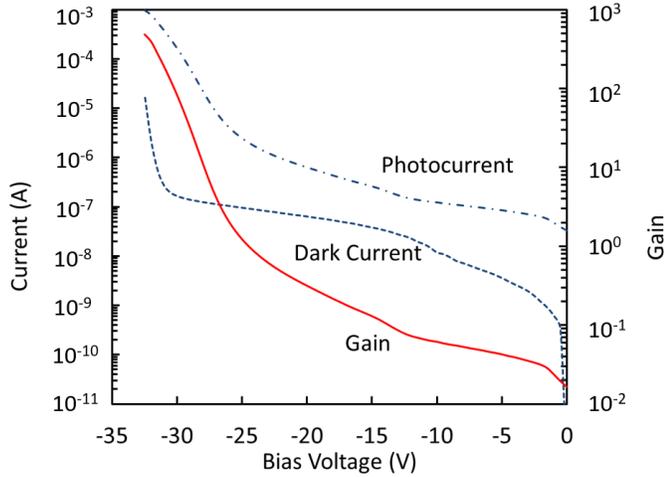


Figure 2. Photocurrent (solid line), dark current (dash dot line), and gain (dash line) versus bias voltage for a 80 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ p-i-n APD.

Since the photocurrent increases continuously with bias and does not exhibit a flat, voltage-independent region, the unity gain point is not obvious. The reason for this is voltage-dependent responsivity at lower bias. Owing to high background doping ($\sim 10^{17} \text{ cm}^{-3}$) in the 1000 nm-thick $\text{Al}_{0.8}\text{InAsSb}$ p⁻ multiplication layer, the carrier collection efficiency improves with increasing bias as the depletion moves closer to the surface. This was confirmed by capacitance-voltage measurements, which were used to calculate the depletion width. Figure 3 shows the capacitance and depletion width versus voltage, where is assumed the dielectric constant of $\text{Al}_{0.8}\text{InAsSb}$ is about 14. And since the device is wet etched, its effective diameter is a little bit smaller than 100 μm , here

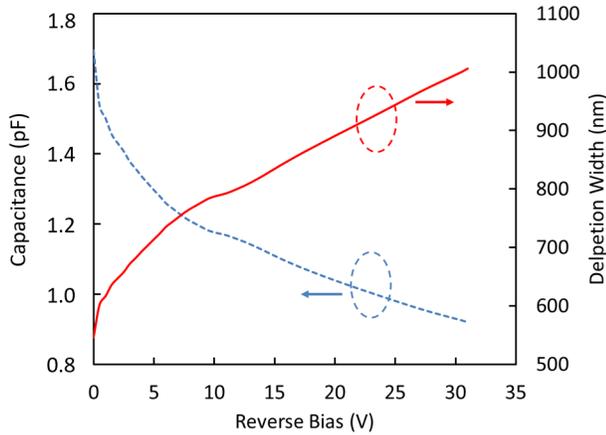


Figure 3. Capacitance and depletion width versus reverse bias of a 100 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ p-i-n APD.

use 98 μm to calculate capacitance.

In order to determine the gain curve in Fig. 2, we have developed a model to fit the external quantum efficiency in order to find the unity gain point. Since the background doping in the multiplication layer is p-type, the edge of the depletion layer will move toward the surface with increasing reverse bias, which, in turn, will result in increased responsivity as more carriers are collected. This is illustrated in Fig. 4.

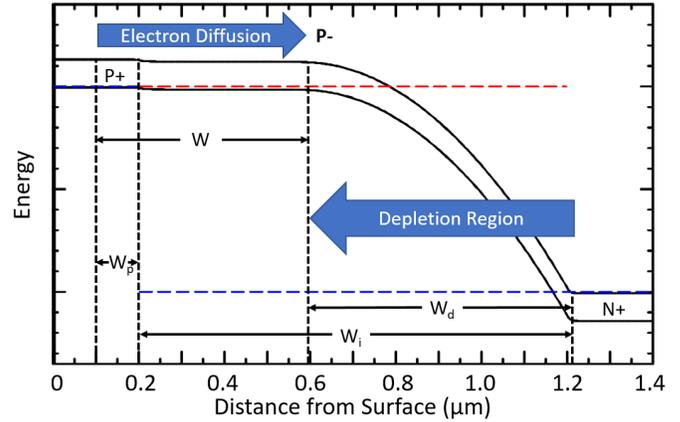


Figure 4. Illustration of mechanism for voltage-dependent responsivity.

The total current density of the device consists the drift current density that is generated in the depletion layer and the diffusion current density that is generated outside the depletion layer and collected by diffusion [13]. The current density can be expressed as:

$$J_{tot} = J_{dr} + J_{diff}, \quad (1)$$

$$J_{dr} = q\Phi_0[\exp(-\alpha W) - \exp(-\alpha W_p - \alpha W_i)], \quad (2)$$

$$J_{diff} = q\left[\frac{\Phi_0\alpha L_n}{1 - \alpha^2 L_n^2} \exp\left(-\frac{W}{L_n}\right) - \frac{\Phi_0\alpha^2 L_n^2}{1 - \alpha^2 L_n^2} \exp(-\alpha W)\right], \quad (3)$$

where the Φ_0 is the incident photon flux per unit area, α is absorption coefficient and L_n is the electron diffusion length. The distance from the surface to the edge of the depletion region, W , can be expressed as $W = W_p + W_i - W_d$, where W_p is the thickness of the $\text{Al}_{0.8}\text{InAsSb}$ p-type layer, W_i is the thickness of the unintentionally-doped multiplication layer, and W_d is the depletion region thickness, respectively.

The total current density can be obtained by substituting eqs. (2) and (3) into eq. (1). The external quantum efficiency can then be calculated using the following equation:

$$\eta_{QE} = (1 - R)(1 - 0.22)\left[\left(1 - \frac{\alpha^2 L_n^2}{1 - \alpha^2 L_n^2}\right) \exp(-\alpha W) + \frac{\alpha L_n}{1 - \alpha^2 L_n^2} \exp\left(-\frac{W}{L_n}\right) - \exp(-\alpha W_p - \alpha W_i)\right], \quad (4)$$

where R is the reflection coefficient of the top surface, about 30%; and 0.22 is the percentage of 850 nm laser absorbed in the top GaSb layer [14]. Figure 5 shows the measured external quantum efficiency of a 200 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ APD versus reverse bias from -1 V to -26 V in 1 V steps. Using eq.

(4) the efficiency at a specific wavelength can be fit with two parameters, α and L_n .

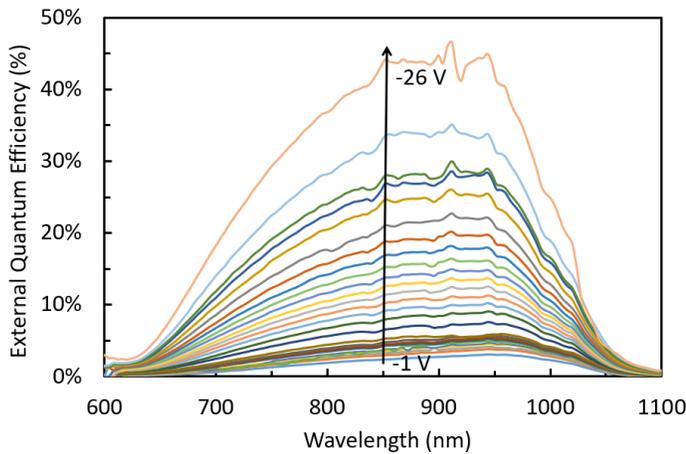


Figure 5. External quantum efficiency of a 200 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ p-i-n APD.

Figure 6 compares the measured and calculated external quantum efficiency at 850 nm for $\alpha = 5.4 \times 10^4 \text{ cm}^{-1}$, $L_n = 170 \text{ nm}$. Using two-parameter curve fitting, good agreement is achieved between the experimental and calculated quantum efficiency up to -24.5 V , which is marked by the dash line. At higher voltage, impact ionization causes the curves to diverge. Therefore, we have used -24.5 V as the unity gain point. After this bias voltage, the multiplication gain dominates the increment of the photocurrent, the change caused by extended depletion region can be ignored. And at that unity gain point the external quantum efficiency is approximately 30% at 850 nm wavelength. The external quantum efficiency is consistent with the photon responsivity from Figure 2, which is about 0.2 A/W .

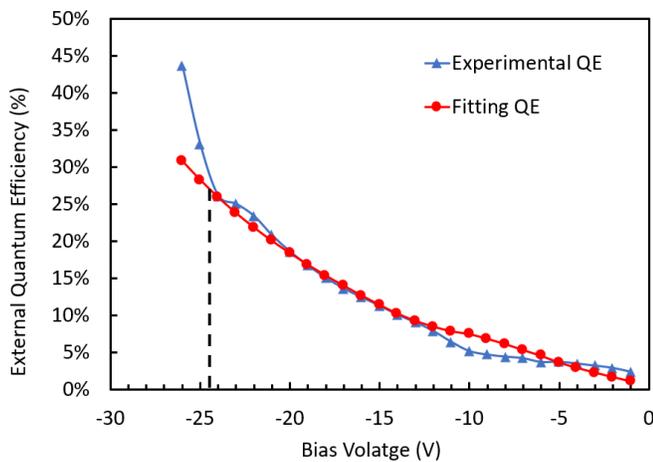


Figure 6. Two-parameter fit of the external quantum efficiency of a 200 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ p-i-n APD at 850 nm wavelength.

The unity gain point can be confirmed and the k value can be determined using a modification of the noise technique described in [15]. The shot noise power is given by [3]:

$$S = 2qI_u M^2 F(M) R(\omega), \quad (5)$$

where I_u is the unity-gain photocurrent, $F(M)$ is the excess noise factor, and $R(\omega)$ is the frequency dependent impedance. From eq. (5), the noise power at any relative gain M_n can be expressed as:

$$S_n = 2qI_u (M_n M_{pt})^2 F(M_n M_{pt}) R(\omega) \quad (6)$$

where M_{pt} corresponds to the gain at the nominal unity-gain point voltage and M_n is the measured gain relative to M_{pt} . We note that M_{pt} may not be exactly unity and its actual value is determined by this procedure. The noise is measured for a series of M_n values and the follow ratio is computed

$$\frac{S_n}{S_{pt}} = M_n^2 \frac{F(M_n M_{pt})}{F(M_{pt})}. \quad (7)$$

The values of S_n and S_{pt} are measured, and the excess noise factors are calculated using the local field model: $F < M > = kM + (1 - k)(2 - 1/M)$. For these measurements based on the discussion above, -24.5 was selected as the M_{pt} reference point. Figure 7 shows the experimental values of S_n/S_{pt} and a fit using M_{pt} and k as adjustable parameters. The best fit was obtained for $M_{pt} = 1.0$, which confirms that -24.5 V is the unity gain point, and $k = 0.05$.

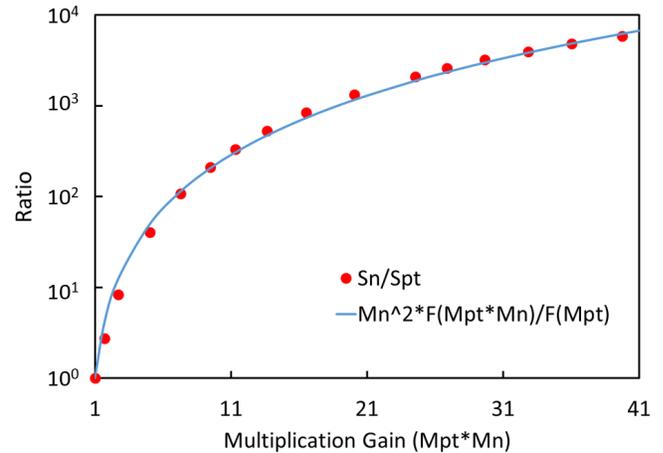


Figure 7. Two-parameters fitting curve of the gain versus ratio of excess noise.

Using -24.5 V as the unity-gain reference, the excess noise was measured with an HP 8970 noise figure meter and a 543-nm He-Ne CW laser [16], [17]. The k value was obtained using the local-field model [3] to plot and the gain values obtained as described above. The data points in Fig. 8 show the excess noise factor versus gain. The value of k is between 0.05 and 0.07 [18], which is consistent with the fitting k value from the Fig. 7.

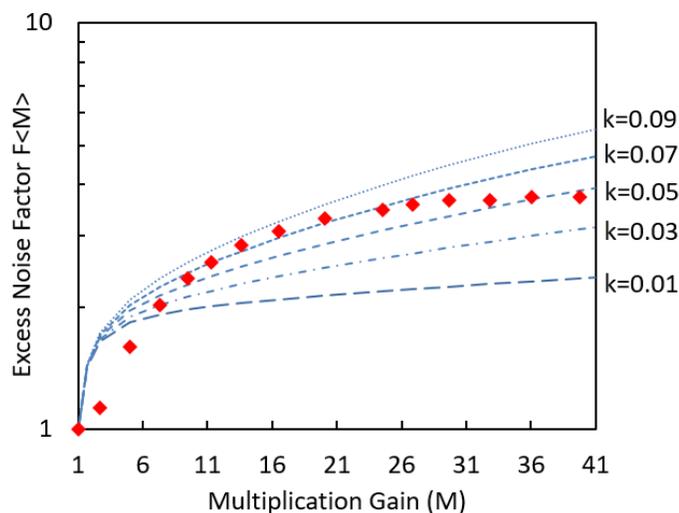


Figure 8. Excess noise factor versus gain of 100 μm -diameter $\text{Al}_{0.8}\text{InAsSb}$ p-i-n APD.

IV. CONCLUSION

We report $\text{Al}_{0.8}\text{InAsSb}$ p-i-n structure APDs, fabricated using the digital alloy growth technique. These APDs exhibit gain as high as 489, low excess noise corresponding to $k = 0.05\text{--}0.07$, and external quantum efficiency of 30% at 850 nm wavelength.

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